

# PRÁCTICA #3 – MEDICIÓN DE FUERZA CON GALGAS EXTENSIOMÉTRICAS

LABORATORIO DE INSTRUMENTACIÓN



# OBJETIVOS

Usar una celda de carga para medición de fuerza aplicada por medios electrónicos (módulo HX711 y Arduino).

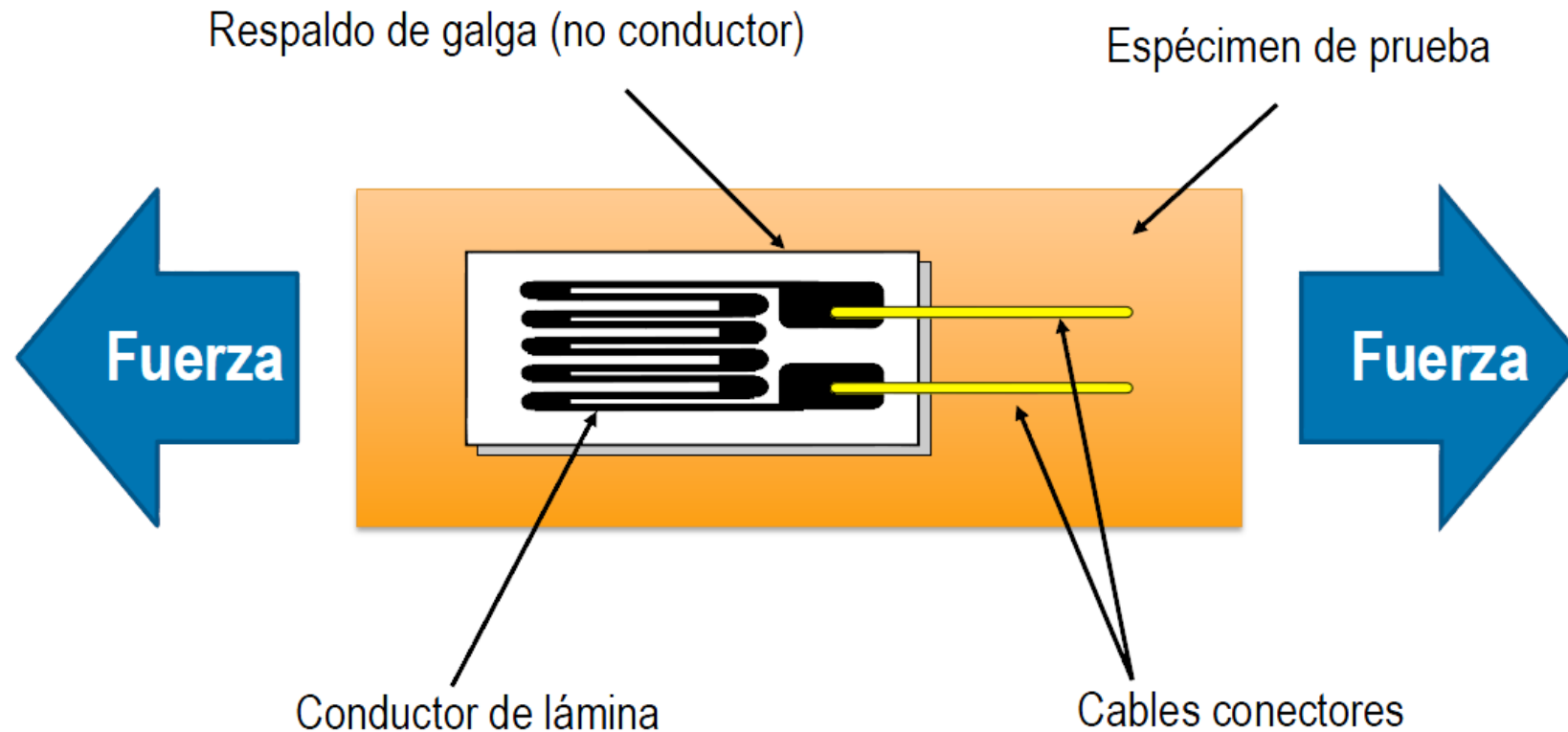
Entender el principio de funcionamiento de la galga extensiométrica en una celda de carga y sus diferentes configuraciones

Caracterizar la respuesta en estado estable del sistema de medición (análisis de histéresis, linealidad, sensibilidad, etc)

Comparar las mediciones hechas con una celda de carga industrial versus una balanza electrónica de bajo costo.



# GALGA EXTENSIOMÉTRICA (PARTES)



# GALGA EXTENSIOMÉTRICA (FUNCIONAMIENTO)

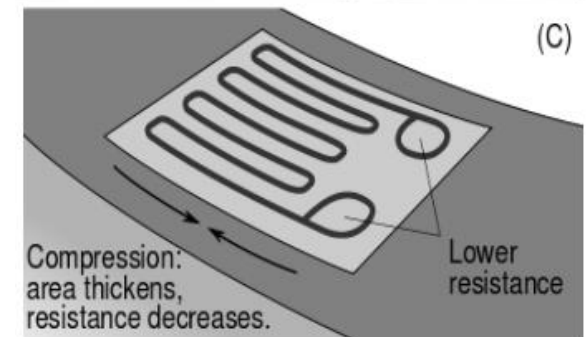
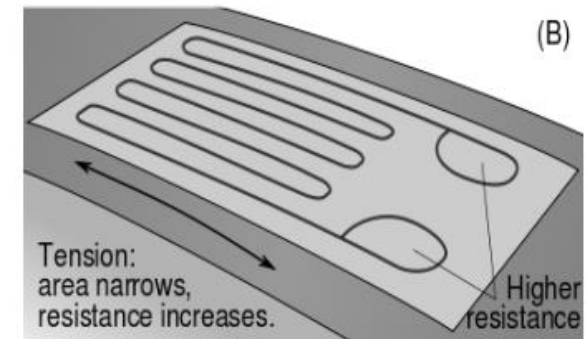
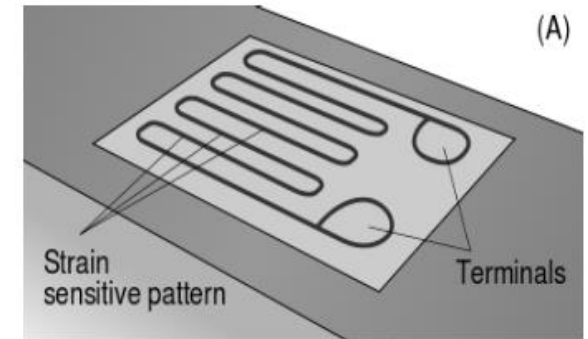
Sensores resistivos variables.

La resistencia varía con respecto a la deformación:

$$\varepsilon = \frac{\Delta L}{L}$$

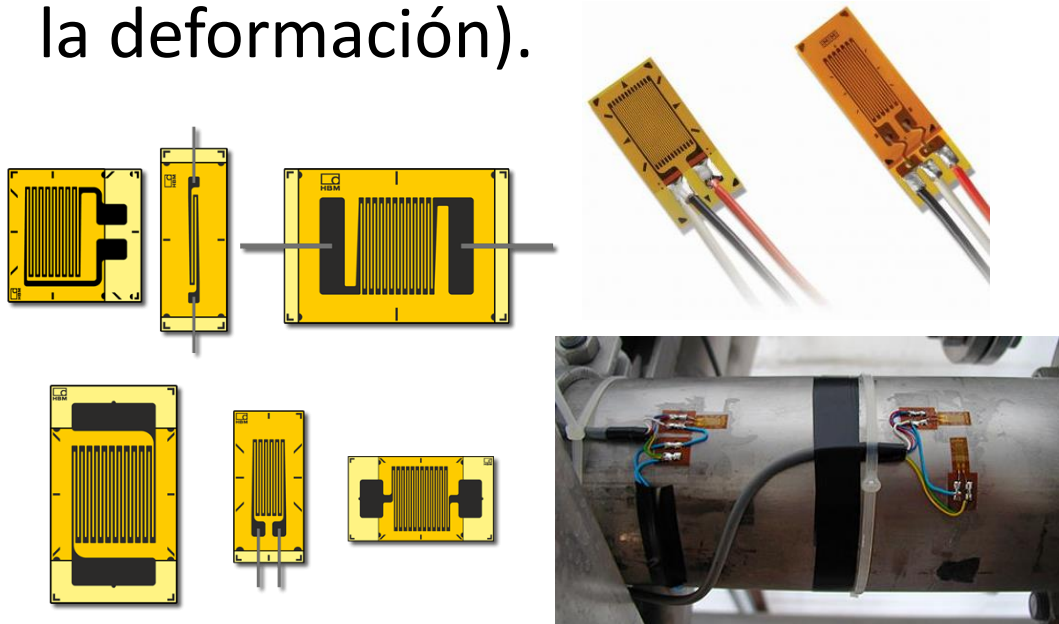
El factor de galga relaciona la tasa de cambio de la resistencia con respecto a la deformación:

$$GF = \frac{\Delta R / R}{\Delta L / L}$$



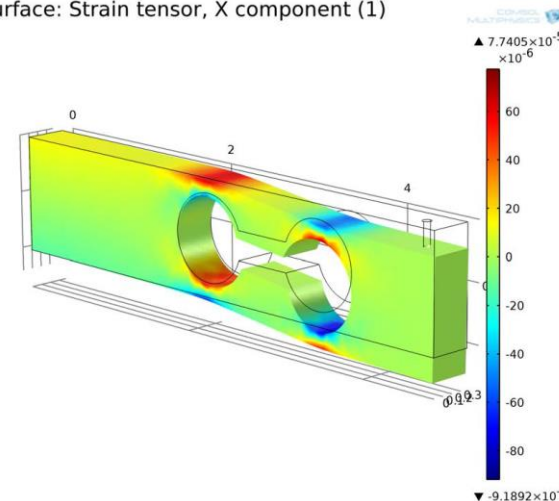
# GALGA EXTENSIOMÉTRICA VS. CELDA DE CARGA

La galga es el transductor resistivo adherido a la probeta o estructura en que se quiere medir la deformación (o cargas que causan la deformación).

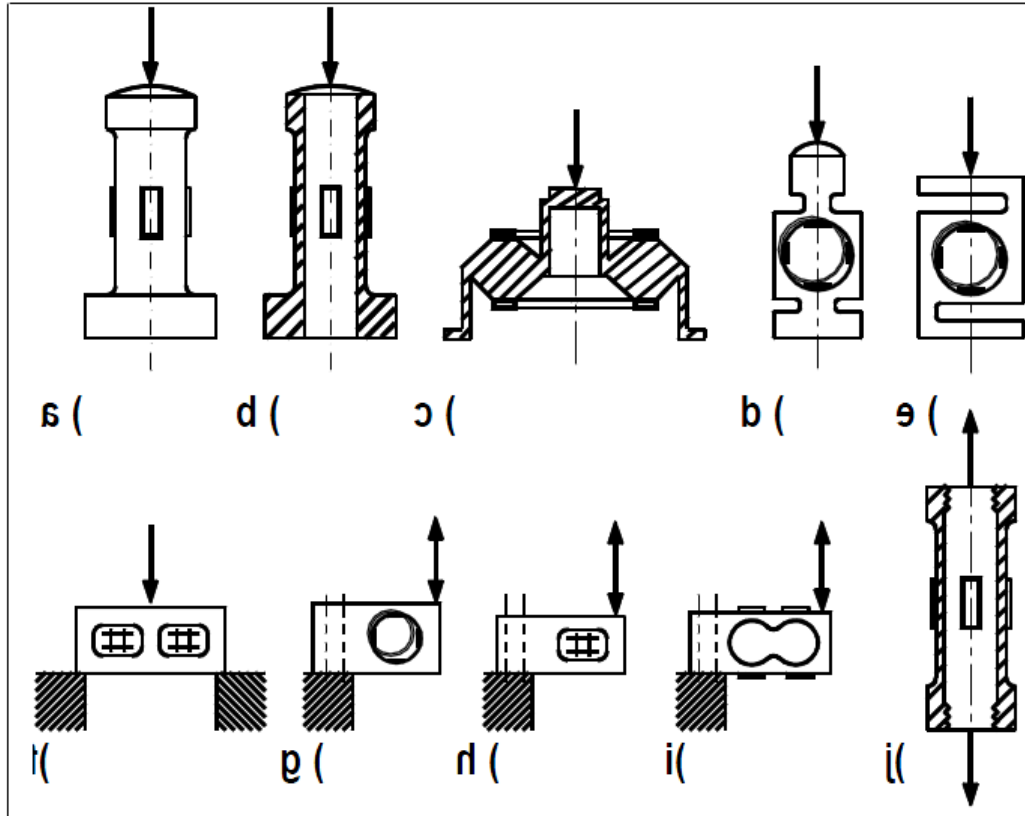


En la celda de carga la probeta (elemento elástico) se diseña para deformarse en cierta medida ante una carga determinada. Se instalan las galgas en las zonas de mayor deformación.

Surface: Strain tensor, X component (1)



# TIPOS DE CELDAS DE CARGA

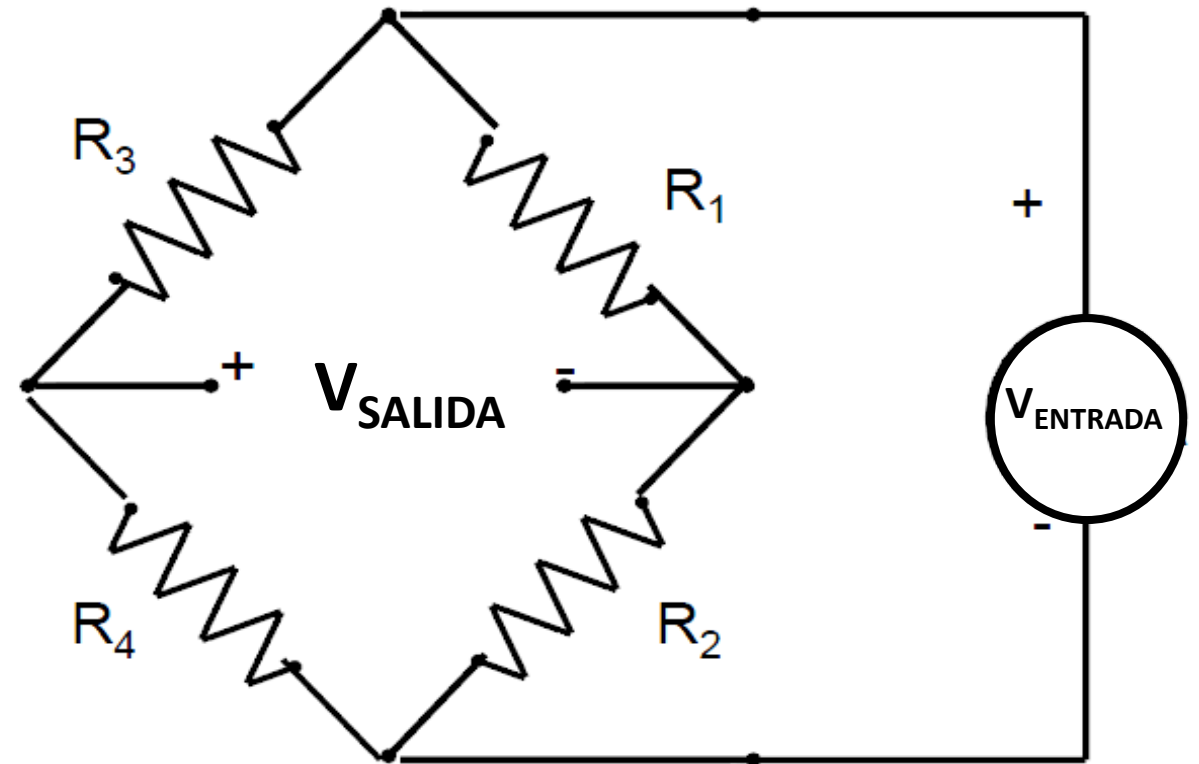
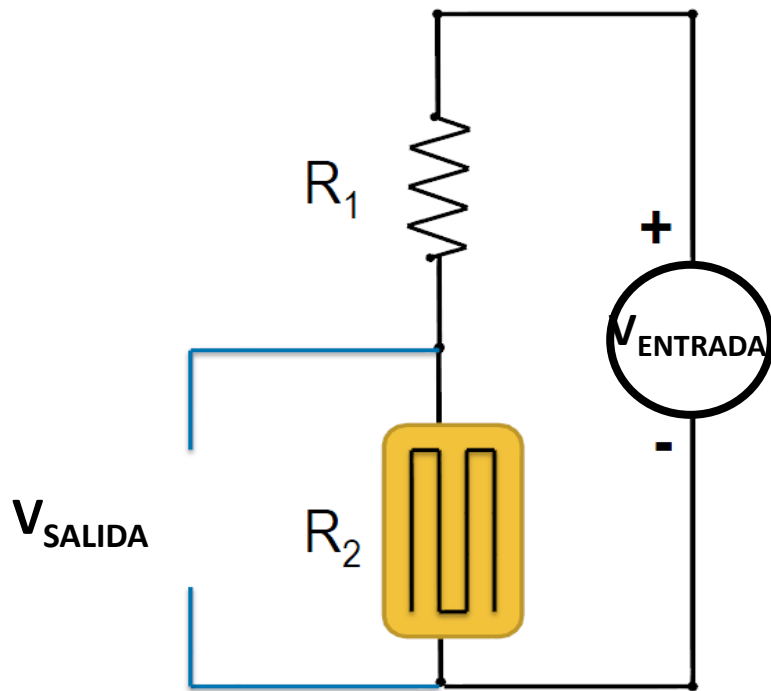


- a) compression cylinder 50 kN to 50 MN
- b) compression cylinder (hollow) 10 kN to 50 MN
- c) toroidal ring 1 kN to 5 MN
- d) ring 1 kN to 1 MN
- e) S-beam (bending or shear) 50 N to 50 kN
- f) double-ended shear beam 20 kN to 2 MN
- g) double-bending beam (simplified) 500 N to 50 kN
- h) shear beam 1 kN to 500 kN
- i) double-bending beam 5 N to 10 kN
- j) tension cylinder 50 kN to 50 MN

# GALGA EXTENSIOMÉTRICA (DIVISOR DE VOLTAJE Y PUENTE DE WHEATSTONE)


$$V_{SALIDA} = V_{ENTRADA} \frac{R_2}{R_1 + R_2}$$

$$V_{SALIDA} = 0 \text{ si } R_1/R_2 = R_3/R_4$$
$$V_{SALIDA} \neq 0 \text{ si } R_1/R_2 \neq R_3/R_4$$



# ERRORES ASOCIADOS A GALGAS

Ruido  Filtrado analógico o digital

Auto-calentamiento  Selección de galga, material base, nivel de excitación, etc

Estabilidad de Voltaje de excitación  Monitoreo del voltaje de excitación

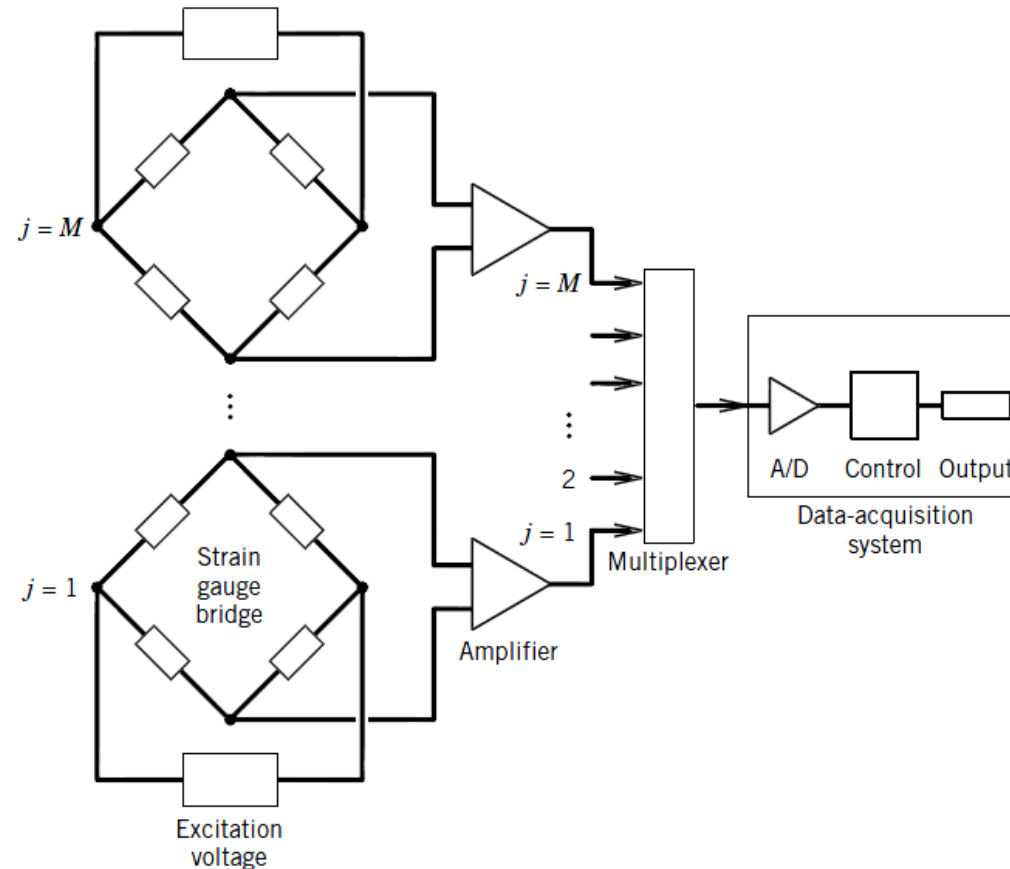
Resistencia de cables largos  Configuración de puente

Problemas de calibración  Calibración del cero y de derivación





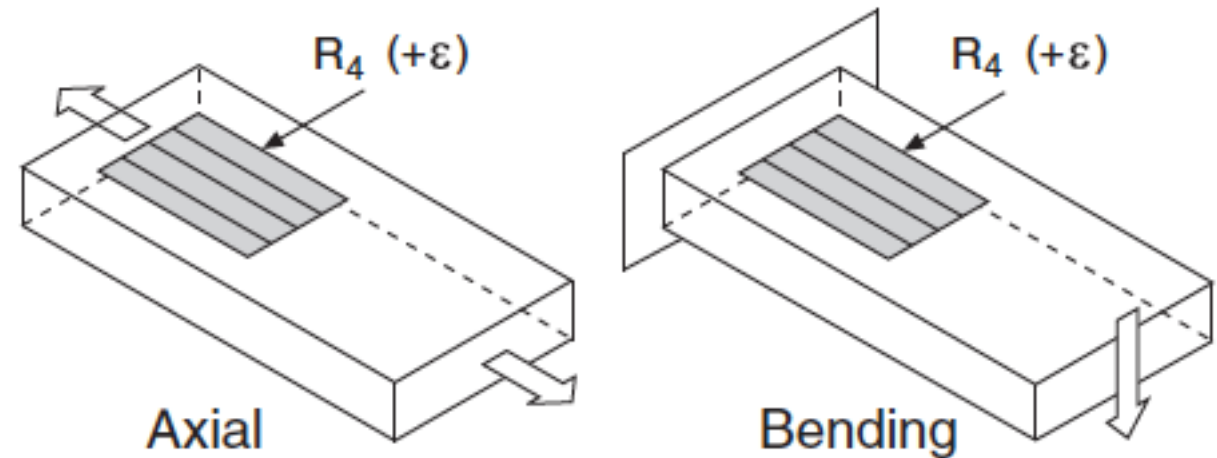
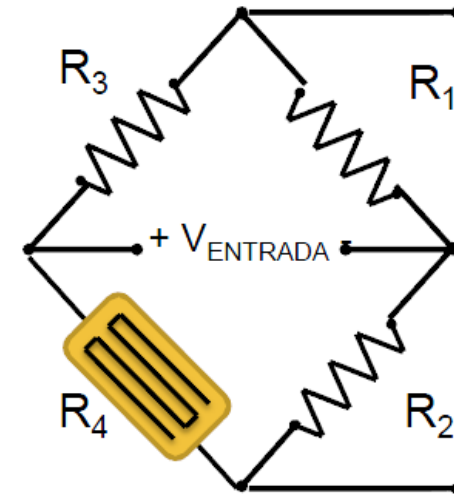
# SISTEMA COMPLETO DE MEDICIÓN



# CUARTO DE PUENTE TIPO I

$$V_r = \frac{V_{O(\text{strained})} - V_{O(\text{unstrained})}}{V_{EX}}$$

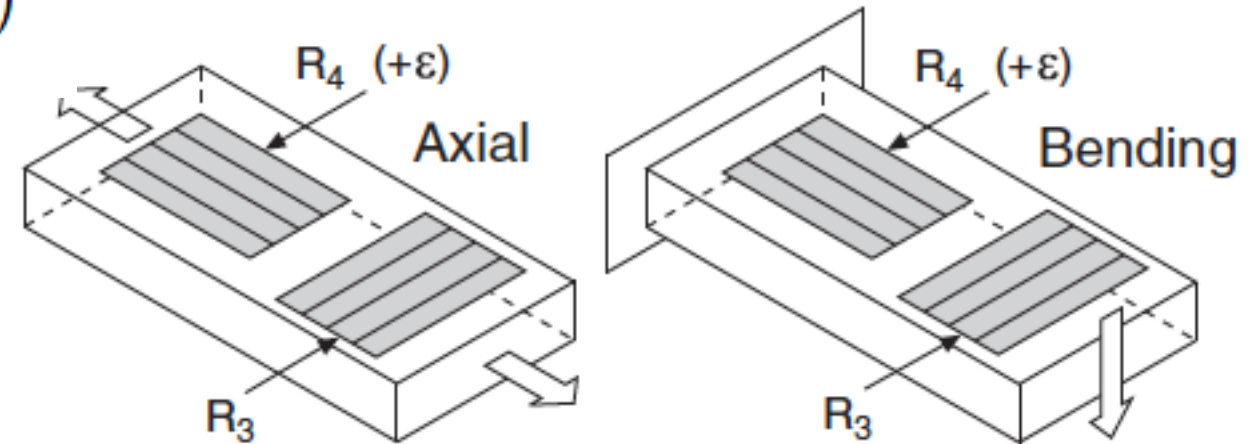
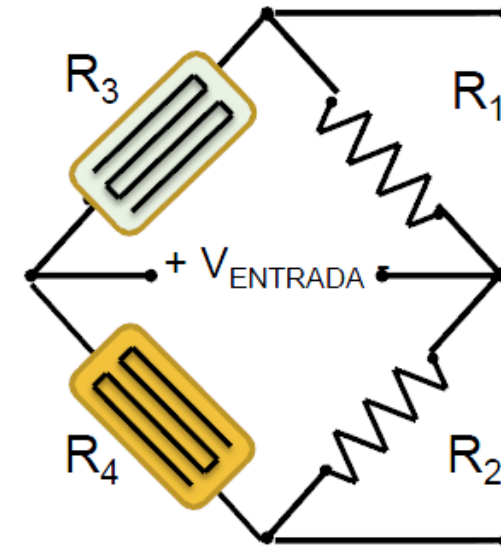
$$\text{strain}(\varepsilon) = \frac{-4V_r}{GF(1 + 2V_r)} \cdot \left(1 + \frac{R_L}{R_G}\right)$$



# CUARTO DE PUENTE TIPO II

$$V_r = \frac{V_{O(\text{strained})} - V_{O(\text{unstrained})}}{V_{EX}}$$

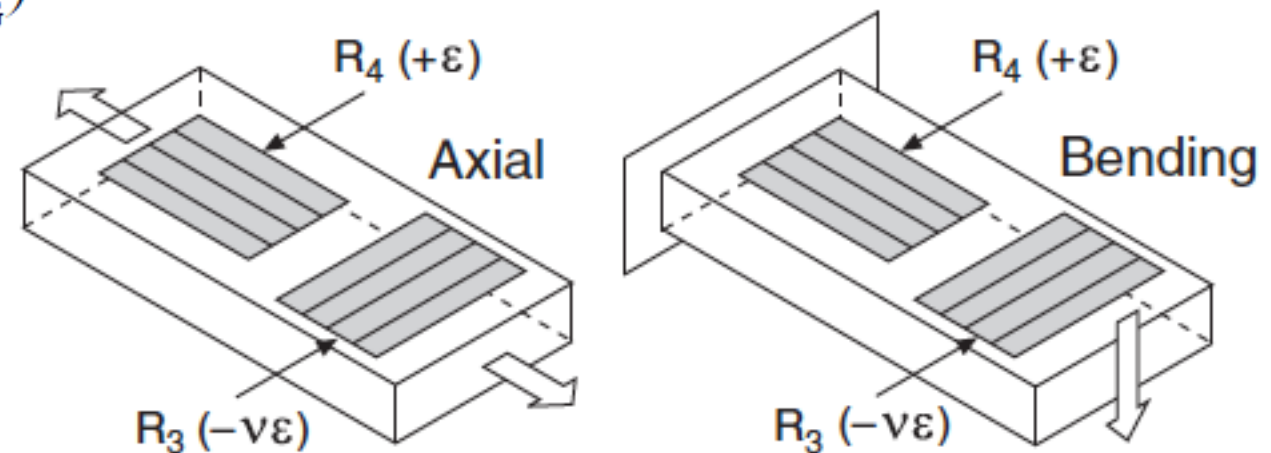
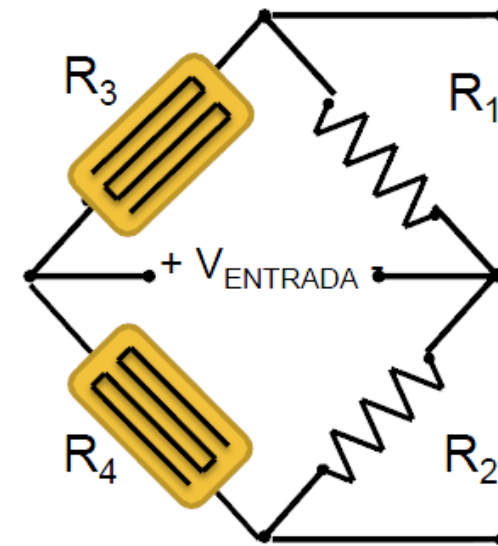
$$\text{strain}(\epsilon) = \frac{-4V_r}{GF(1 + 2V_r)} \cdot \left(1 + \frac{R_L}{R_G}\right)$$



# MEDIO PUENTE TIPO I

$$V_r = \frac{V_{O(\text{strained})} - V_{O(\text{unstrained})}}{V_{EX}}$$

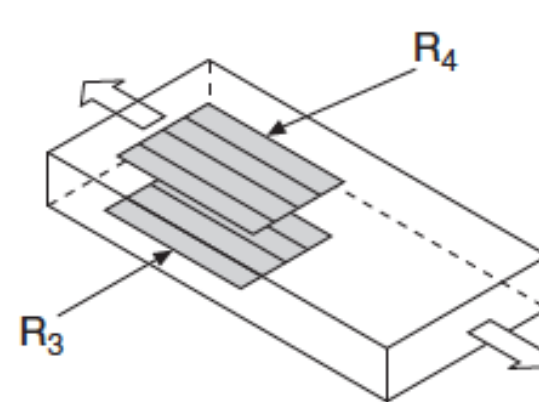
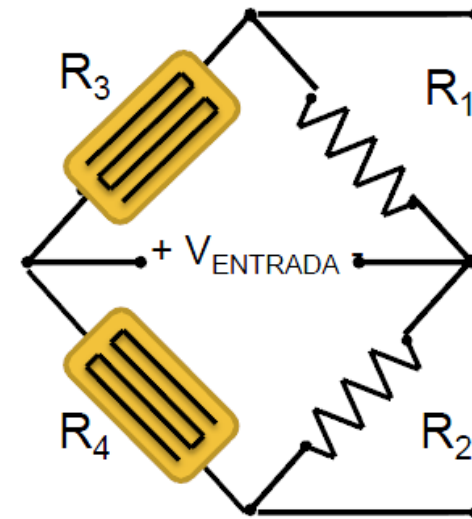
$$\text{strain}(\epsilon) = \frac{-4V_r}{GF[(1 + \nu) - 2V_r(\nu - 1)]} \cdot \left(1 + \frac{R_L}{R_G}\right)$$



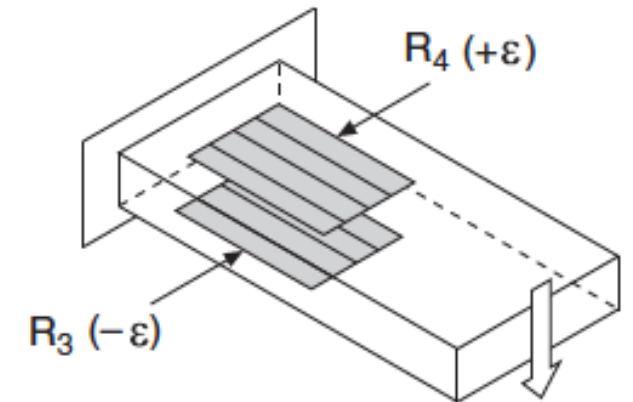
# MEDIO PUENTE TIPO II

$$V_r = \frac{V_{O(\text{strained})} - V_{O(\text{unstrained})}}{V_{EX}}$$

$$\text{strain}(\epsilon) = \frac{-2V_r}{GF} \cdot \left(1 + \frac{R_L}{R_G}\right)$$



Rejects Axial

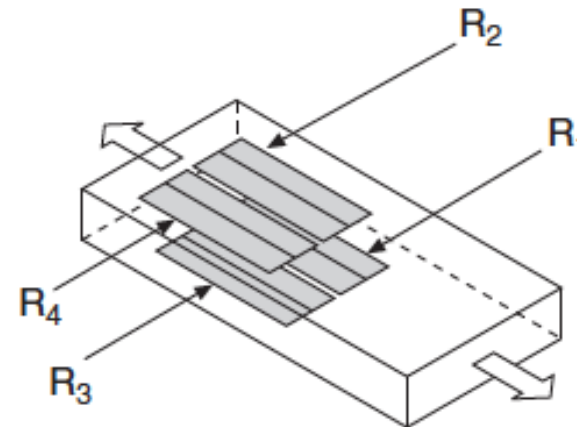
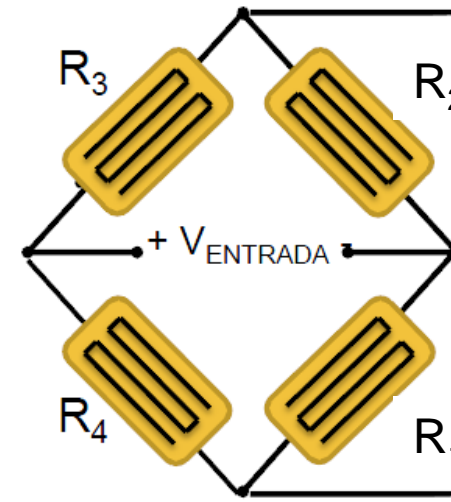


Measures Bending

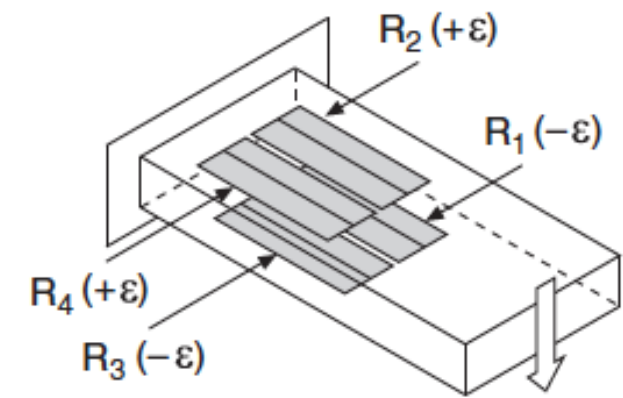
# PUENTE COMPLETO TIPO I

$$V_r = \frac{V_{O(\text{strained})} - V_{O(\text{unstrained})}}{V_{EX}}$$

$$\text{strain}(\varepsilon) = \frac{-V_r}{GF}$$



Rejects Axial

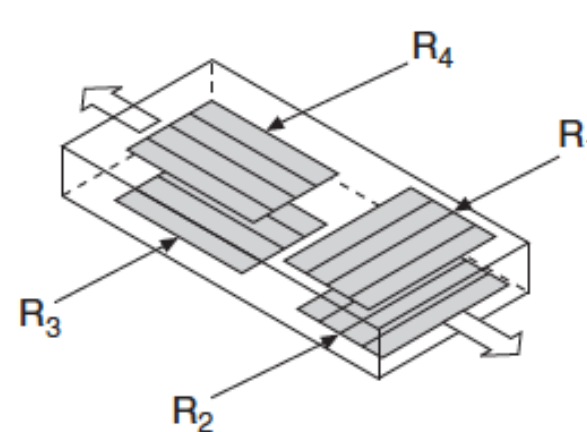
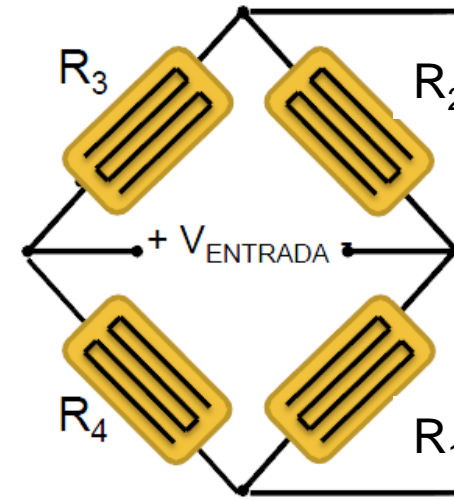


Measures Bending

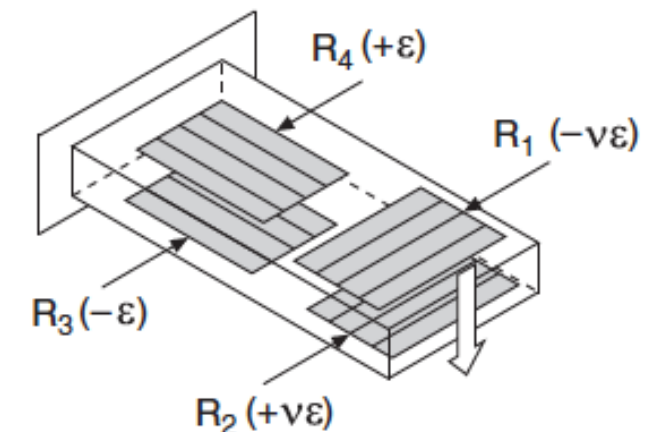
# PUENTE COMPLETO TIPO II

$$V_r = \frac{V_{O(\text{strained})} - V_{O(\text{unstrained})}}{V_{EX}}$$

$$\text{strain}(\varepsilon) = \frac{-2V_r}{GF(\nu + 1)}$$



Rejects Axial

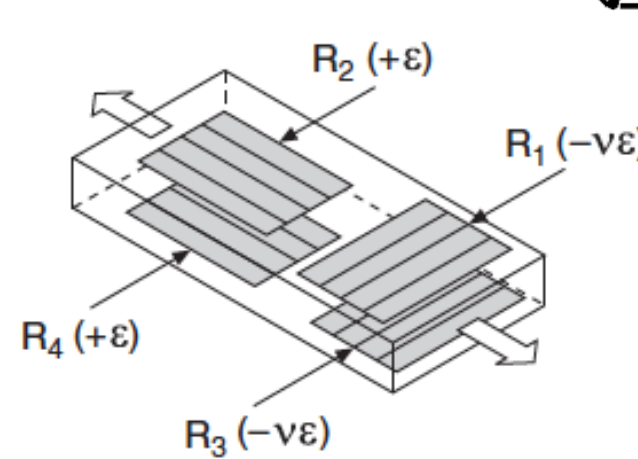
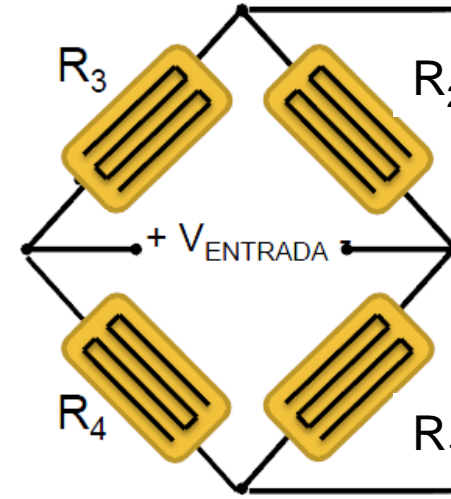


Measures Bending

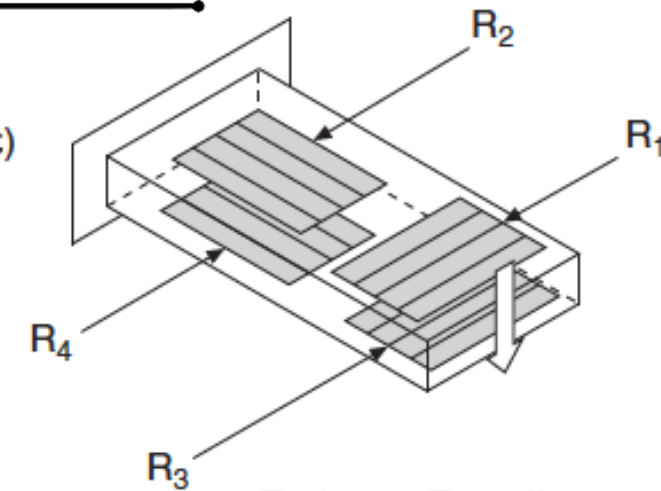
# PUENTE COMPLETO TIPO III

$$V_r = \frac{V_{O(\text{strained})} - V_{O(\text{unstrained})}}{V_{EX}}$$

$$\text{strain}(\varepsilon) = \frac{-2V_r}{GF[(\nu + 1) - \nu_r(\nu - 1)]}$$



Measures Axial



Rejects Bending



# HOJA DE DATOS DE GALGA EXTENSIOMÉTRICA

EA-13-240LZ-120  
Gage Type

---

120.0 ± 0.3%  
Resistance in Ohms

---

2.09 ± 0.5%  
Gage Factor at 75°F

---

+0.8%  
K<sub>t</sub>

---


E  
Option

---

R-A41AF58  
Lot Number

---

963914  
Code

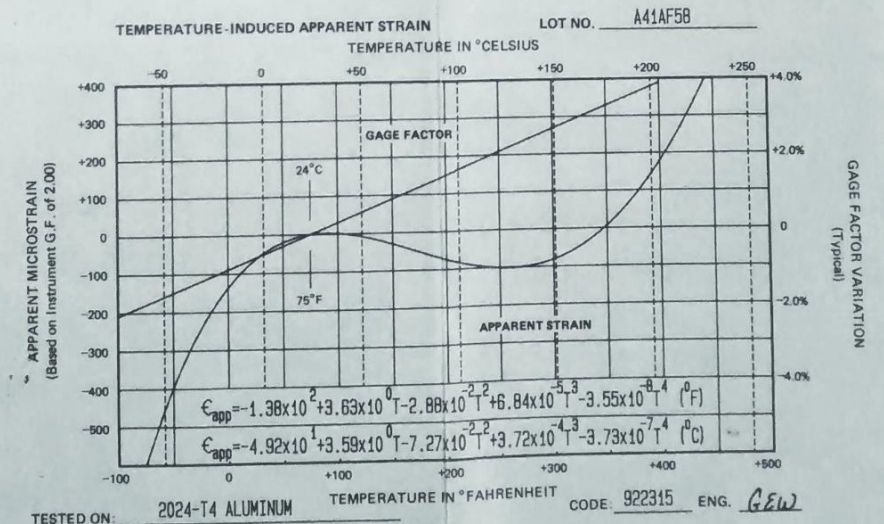


Micro-Measurements  
Division

**MEASUREMENTS  
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Raleigh, North Carolina 27611  
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**SELF-TEMPERATURE COMPENSATION:** These gages have been manufactured with self-temperature compensation (STC) characteristics to minimize apparent strain (see Tech Note TN-504). Apparent strain data given below are valid only for the indicated test material, since thermally-induced apparent strain is a function of the thermal expansion properties of the test specimen.



# HOJA DE DATOS DE CELDA DE CARGA

## SPECIFICATIONS

**Excitation:** 5 Vdc, 15 Vdc maximum

**Output:** 1 mV/V  $\pm$  0.1%

**Linearity:**  $\pm$  0.02% FS

**Hysteresis:**  $\pm$  0.01% FS

**Zero Balance:**  $\pm$  5% FS

**Creep (in 30 minutes):**  $\pm$  0.03% FS

**Operating Temp Range:** -10 to 100°C  
(14 to 212°F)

**Compensated Temp Range:**  
-10 to 100°C (14 to 212°F)

### Thermal Effects:

**Span:**  $\pm$  0.005% FS/°C (0.003/°F)

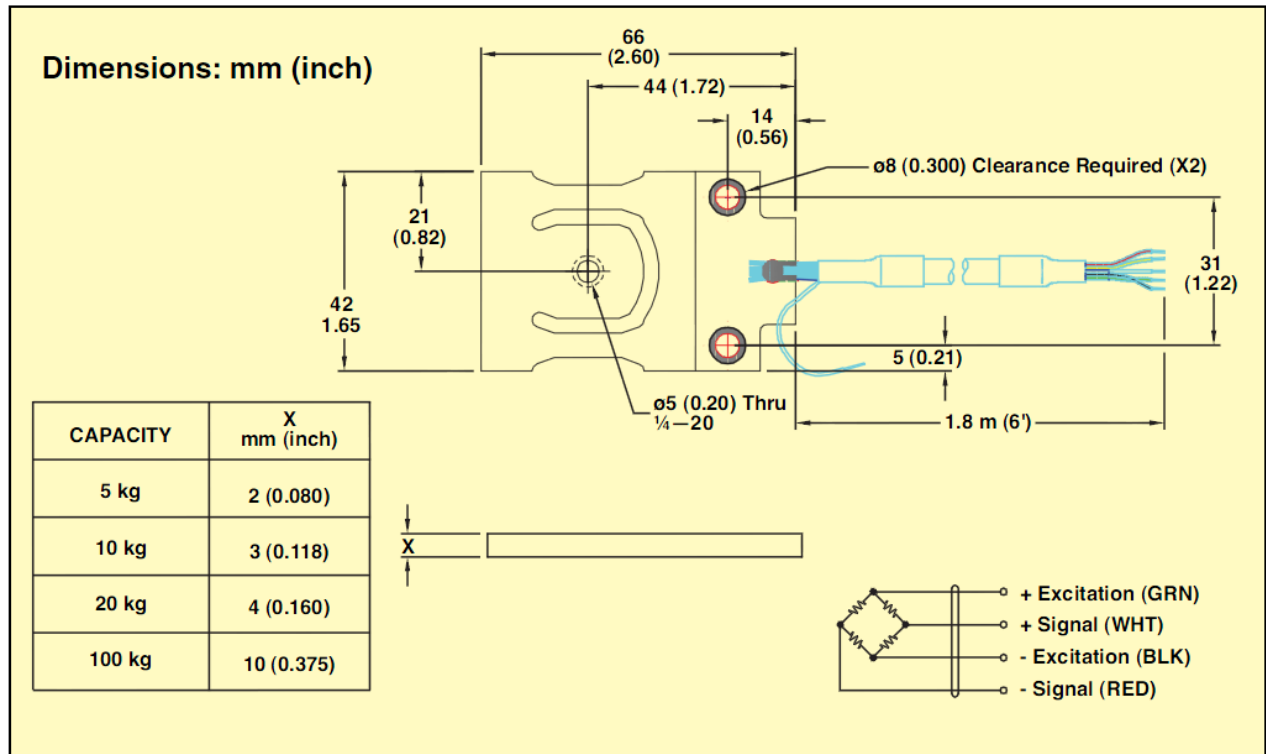
**Zero:**  $\pm$  0.005% FS/°C (0.003/°F)

**Safe Overload:** 300% of capacity

**Ultimate Overload:** 400% of capacity

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CAPACITY		MODEL NO.	"X" DIMENSION mm (inch)	COMPATIBLE METERS
kg	lb			
100	220	LCPB-100	9.53 (0.375)	DP25B-S, DP41-S, DPiS



# ¿PREGUNTAS?

